

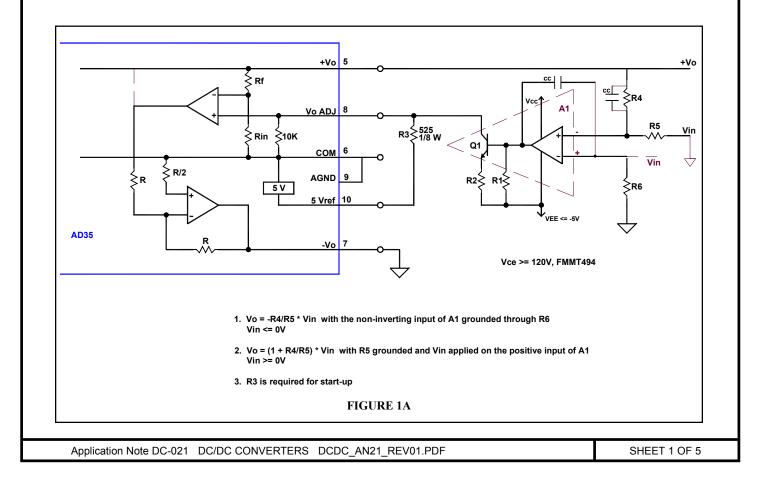
## PROGRAMMING THE AD35 DC/DC CONVERTER

Referring to Figure 1A, amplifier A1 consists of a low voltage op amp and a high voltage NPN transistor Q1. By grounding the negative output of the AD35, the converter operates as a single positive output DC/ DC from 0 to 200V.

A1 through Q1 sets the V<sub>o</sub> ADJ voltage of AD35. At turn on, the 5V<sub>REF</sub> of the converter through R3 will set the output to 200V if A1 is not powered up (V<sub>CC</sub> = V<sub>EE</sub> = 0). When V<sub>CC</sub> and V<sub>EE</sub> of A1 is turned on at the same time, the AD35 is turned on and A1 takes over the control of the output of AD35. A1 will wait for a few milliseconds due to the turn on delay and soft start of the AD35.

It must be pointed out that the AD35 operates as a non-inverting amplifier, i.e.  $V_{out}$  increases as  $V_o$  ADJ increases or, more specifically,  $V_o$  ADJ increases with respect to  $V_o$  COM. Therefore an inverting amplifier can be used to control the AD35. In this configuration,

the voltage gain of the linear block is given by the feedback resistor network R4 and R5. The linear block of A1 plus AD35 can be viewed as a single positive supply, adjustable amplifier that can be controlled through a positive input when  $V_{IN}$  is applied on the non-inverting input of A1 (the negative input of the op amp inside A1) or through a negative  $V_{IN}$  when the positive input of A1 is grounded through R6 and -  $V_{IN}$  is applied at the open end of R5. As can be seen in Figure 1A, R1 and R2 are pull-down resistors to  $V_{EE}$ . Depending on the voltage used for  $V_{EE}$ , select R2 such that  $V_{c}$  of Q1 is a few millivolts (mV) negative when  $V_{o} = 0V$  and Q1 is at saturation. The collector current of Q1 is the current through R3 required to set  $V_{o}$  ADJ to 0V.



5V/R3 = I <= 9.5mA

and

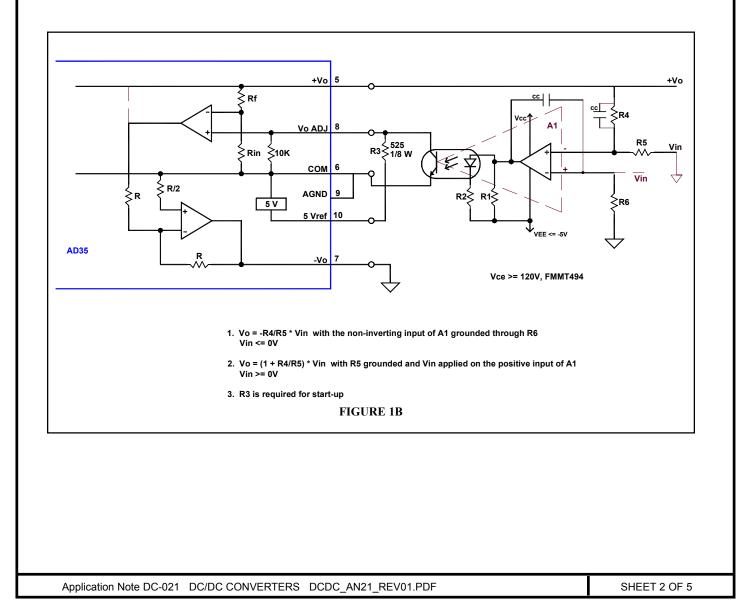
$$V_{ce} + I^*R^2 = V_{ee}$$

For  $V_{CE}$  of Q1 = 100mV,  $V_{EE}$  = -5V, I = 9.6mA

 $R2 = (5 - 0.1)/9.6 = 510\Omega$ 

R1 is required only if the output voltage of the selected amplifier inside A1 cannot go rail to rail such as LM358, MC34072 and others. R1 will pull the output to  $V_{\text{EE}}$  forcing Q1 off and the collector current to zero when +V<sub>o</sub> is set for the V<sub>o</sub> maximum of 200V.

A photo coupler can also be used as the output stage of A1 to replace Q1 (see Figure 1B). The collector of the phototransistor is connected to  $V_o$  ADJ (Pin 8 of AD35) while the photodiode will be connected as is to the emitter of Q1 (between R2 cathode and the output of the OPAM inside A1 anode). The accuracy of the linear block depends only on the accuracy of  $V_{IN}$  and its feedback network R4 and R5.

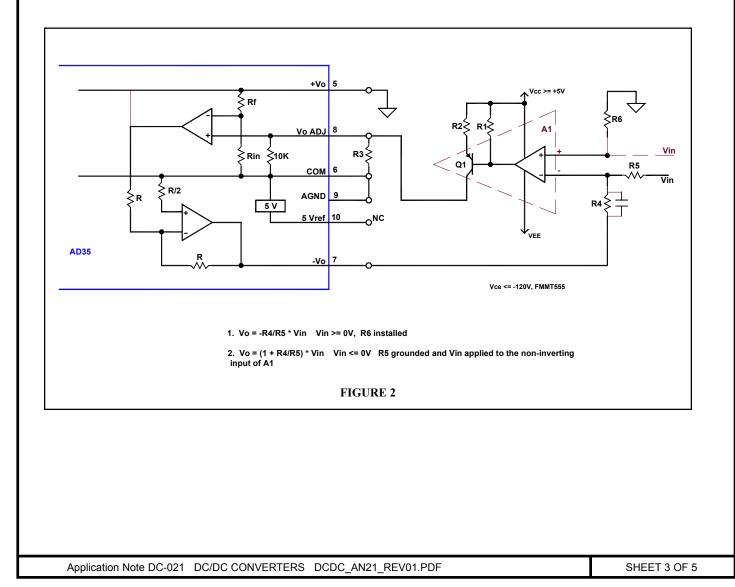


Referring to Figure 2, the AD35 with A1 is configured as a single negative, adjustable output converter. The positive output (Pin 5) is grounded and the rest of the output pins are floating.

At turn on, if A1 is not powered up, the output of AD35 will be zero volts (0V). The AD35 block behaves as an inverting amplifier in Figure 2 (i.e.  $-V_{\odot}$  increases as  $V_{\odot}$  ADJ Pin 8 becomes more positive with respect to COM Pin 6 or as the collector current through Q1 increases).

Given that the AD35 block acts as an inverting amplifier and Q1 also acts as an inverting amplifier, the input pin polarity of A1, inverting and non-inverting inputs, and the op amp inside A1 have the same polarity, then the negative output  $V_o$  at Pin 7 is given as:  $-V_o = (R4/R5)V_{IN}$  with the non-inverting input grounded through R6 and  $V_{IN} >= 0$ . With R5 connected to ground and  $V_{IN}$  applied at the non-inverting input,  $V_o = (1+(R4/R5))V_{IN}$  for  $V_{IN} <= 0$ .

R3 in Figure 2 can be connected between V<sub>o</sub> ADJ Pin 8 and COM (in parallel with 10K) when higher current through Q1 is required to increase noise immunity or resolution. R1 performs the same function as described above in Figure 1A. If a photocoupler is used (as it is shown in Figure 1B) to replaced Q1 in Figure 2, the collector of the phototransistor is connected at the 5V<sub>REF</sub> Pin 10 and its emitter at V<sub>o</sub> ADJ Pin 8. The photodiode of the optocoupler will replace the emitter to base function of Q1 in Figure 2. A dual operational amplifier and two bipolar high voltage transistors can be used to design a bipolar adjustable 0 to ±200V voltage source, which can be controlled from a single input voltage source.



## Programming the AD35 with a Current Source

Referring to Figure 3, a current source with open circuit protection is used to program the positive output voltage of the AD35. The D/A converter through A1 and Q1 sets the current through RCS, which is given by:  $I = (V_{D/A})/R_{CS}$ .

The open circuit protection consists of A2 with its input network and Q2. When S1 is set to the off position,  $V_B$  drops to 0V, comparator A2 turns Q2 on setting the positive input of A1 to 0V. Without the open circuit protection and if  $V_{DS}$  is 0V, the output of A1 will go to its maximum output voltage, turn on Q1 and stay at its maximum  $V_{OUT}$  until  $V_{DS}$  is connected to a voltage source or S1 is set to the on position.

As soon as  $V_{DS} > 0$ , Q1 will be fully on and the only current limiting resistor will be  $R_{CS}$ . Because A1 does not respond instantaneously, the unlimited current through  $R_{CS}$  may destroy  $R_{CS}$  and force the  $V_O$  ADJ voltage at Pin 8 to momentarily go to zero or even cause the output of the AD35 to become unstable.

OFF

S

ON

Vx or

The voltage divider for V<sub>B</sub> must be very high (in the order of M $\Omega$ ) to allow a very small amount of current through it. To calculate the current I versus V<sub>o</sub> from the AD35 data sheet:

#1 
$$V_0 = 42*V_0 ADJ$$

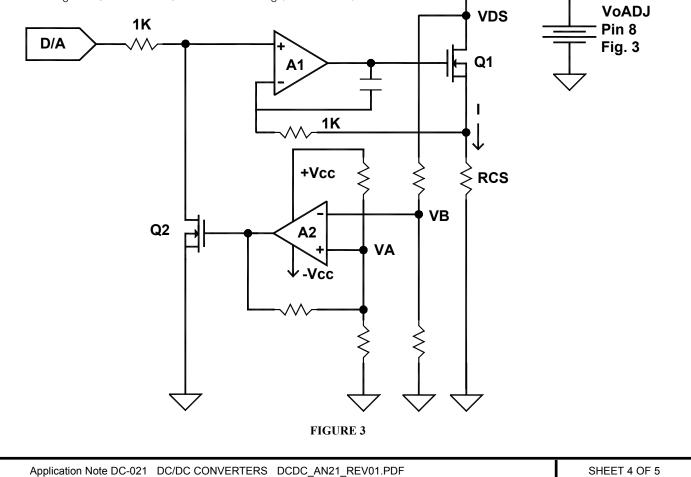
and from Figure 1A,

#2  $V_{o} ADJ = 5V - R3^*I$  (if we neglect the 10k $\Omega$ )

#3 
$$V_{o} = 42(5 - R3*I) = 210 - 42R3*I$$

#4 I = 
$$(V_0 - 210)/(42*R3) = (V_0 - 210)/22050$$

where  $V_{o}$  in Eq. 4 is the required value for  $V_{o}$  (Pin 5 AD35).



Referring to Figure 4, the AD35 is connected for a negative output. The current source consists of A1, a P-channel high-voltage MOSFET and a stable voltage source  $V_x$ . From the data sheet,  $V_0$  is given by:

#2  $V_o ADJ = 10^* I \text{ or } (10||R_x)^* I$  if  $R_x$  is installed  $I = (V_x - V_{D/A})/R_{CS}$ 

If an open circuit protection is needed, the same approach used in Figure 2 will force  $V_{D/A}$  to  $V_{x}$ , thus the current through  $R_{cs}$  will be zero.

